

К вопросу о сортировке пиломатериалов по качественному признаку

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On the issue of sorting sawn timber according to the quality criteria

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In the article the question of sorting of saw-timbers from wood on a qualitative basis is investigated. The consideration of all types of forest products from the positions of applied system analysis reveals several interesting features of these research objects. On the one hand, they are an artificial scientific object (in terms of dimensional parameters) and at the same time preserve the attributes of a natural scientific object in terms of their qualitative parameters. It is also remarkable that this feature is manifested not only in a combination of logs or boards (blanks), but also in each individual object. It is this feature that explains all the difficulties associated with the evaluation of quality and the sorting of forest products. Previous theoretical studies in the field of assessing the quality of sawmill showed that the purpose of the product should be taken as the basis for a new approach. When sorting sawmill products by designation, the main indicator is the internal non-uniformity of the board, which was not previously investigated. The article describes the results of experimental studies examining the internal heterogeneity of sawmilling as an assumed basis for grade evaluation. For research, pine and spruce sawmills of a certain range of sections were taken. The four timber surfaces (both plates and longitudinal edges), which can have different wood defects, were examined. The localization, dimensions and quantity of defects are the initial information for cutting and sorting operations. The possible correlation of grades on each of the four sides of the cross-section of a single board was studied. The obtained results can be used to improve the system of quality standards for sawn timber.

Keywords: wood defects; sawn timber; quality control.

/	1-	1-	2-	2-	d	d ²
1	0	9	0	10,5	-1,5	2,25
2	1	19,5	0	10,5	9	81
3	0	9	0	10,5	-1,5	2,25
4	0	9	0	10,5	-1,5	2,25
5	0	9	0	10,5	-1,5	2,25
6	0	9	0	10,5	-1,5	2,25
7	0	9	0	10,5	-1,5	2,25
8	0	9	0	10,5	-1,5	2,25
9	0	9	0	10,5	-1,5	2,25
10	0	9	0	10,5	-1,5	2,25
11	0	9	0	10,5	-1,5	2,25
12	0	9	0	10,5	-1,5	2,25
13	0	9	0	10,5	-1,5	2,25
14	1	19,5	0	10,5	9	81
15	0	9	0	10,5	-1,5	2,25
16	1	19,5	0	10,5	9	81
17	0	9	0	10,5	-1,5	2,25
18	0	9	0	10,5	-1,5	2,25
19	1	19,5	1	10,5	-1,5	2,25
20	0	9	0	10,5	-1,5	2,25
21	0	9	0	10,5	-1,5	2,25
						283,5

[8-10]:

$$r_s = 1 - 6 \cdot \frac{\sum d^2}{N \cdot (N^2 - 1)}, \quad (1)$$

$$U' = \frac{1}{12} \sum_t (u^3 - u). \quad (3)$$

d² —

; N —

. 4)

t u

(1)

0,768.

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$$T' = \frac{1}{12} \sum_t (t^3 - t), \quad (2)$$

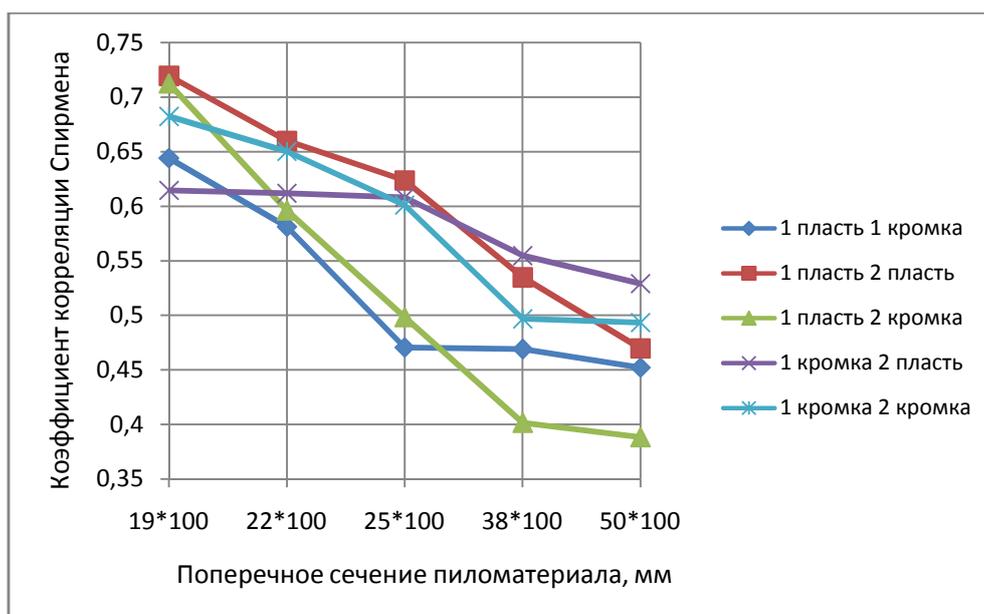
$$r_s = 1 - 6 \cdot \frac{\sum d^2 + T' + U'}{N \cdot (N^2 - 1)}. \quad (4)$$

. 4 (4),

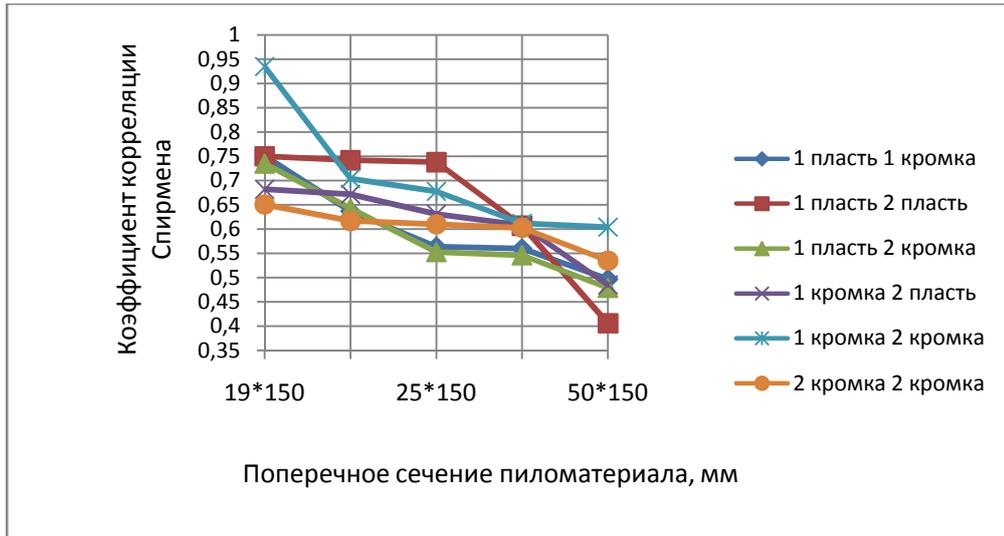
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/	1- 1-	1- 2-	1- 2-	1- 2-	1- 2-	2- 2-
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50*150	0,497	0,406	0,479	0,485	0,604	0,535
38*150	0,560	0,607	0,580	0,608	0,612	0,603
25*150	0,564	0,738	0,531	0,631	0,678	0,610
22*150	0,637	0,742	0,643	0,672	0,704	0,617
19*150	0,751	0,744	0,735	0,682	0,935	0,651
50*100	0,452	0,470	0,388	0,529	0,493	0,580
38*100	0,469	0,535	0,390	0,555	0,497	0,583
25*100	0,471	0,624	0,498	0,608	0,601	0,591
22*100	0,581	0,660	0,596	0,612	0,650	0,595
19*100	0,644	0,719	0,712	0,615	0,682	0,599
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50*150	0,488	0,412	0,463	0,458	0,602	0,565
38*150	0,515	0,637	0,542	0,610	0,610	0,625
25*150	0,524	0,704	0,557	0,612	0,648	0,632
22*150	0,597	0,716	0,656	0,629	0,698	0,648
19*150	0,698	0,782	0,756	0,655	0,875	0,695
50*100	0,399	0,486	0,352	0,612	0,475	0,569
38*100	0,545	0,595	0,581	0,626	0,548	0,596
25*100	0,576	0,626	0,589	0,651	0,658	0,599
22*100	0,581	0,644	0,612	0,675	0,680	0,615
19*100	0,594	0,672	0,674	0,685	0,722	0,619



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